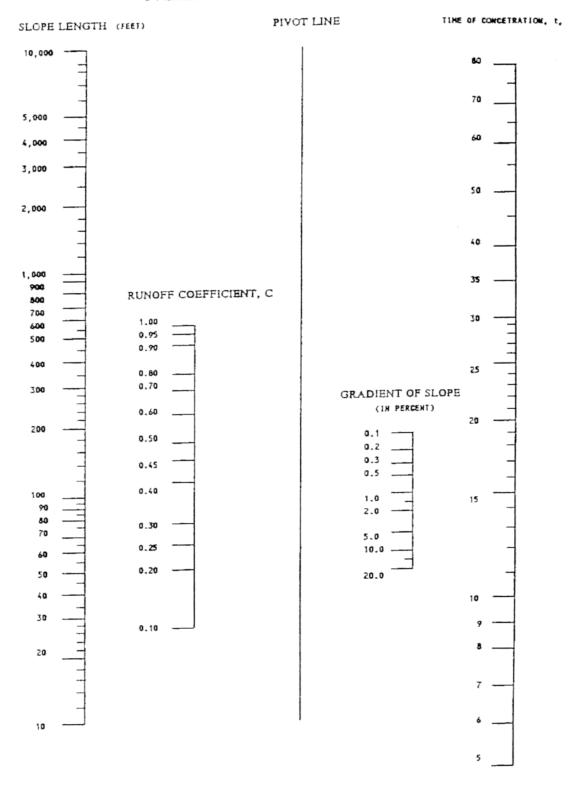
#### OVERLAND FLOW CHART



### Worksheet 2: Runoff curve number and runoff

Project(			Ву		Date			
			ted					
Circle one: Pres	sent Developed							
1. Runoff curv	ve number (CN)							
Soil name and hydrologic	Cover description		CN <u>1</u> /	′	Area		Product of CN % area	
group	(cover type, treatment, and hydrologic				□ acres □ mi <sup>2</sup>			
(Appendix A)	endix A) condition; percent impervious; unconnected/connected impervious area ratio)		Table 2-2 Fig. 2-3 Fig. 2-4		□ %			
						_		
						_		
1/ Use only one CN s	source per line	Tota	als =					
CN (weighted) = to 2. Runoff	otal product/total area =; U	Jse Cl	N =					
Frequency	yr		Stori	m #1	Storm #2	Stor	rm #3	
Rainfall, P (24-hou	ır)in							
	with table 2-1, fig. 2-1, or eqs.							

### Worksheet 3: Time of concentration $(T_c)$ or travel time $(T_t)$

Proje	ct				l	3y	Date _	
Locat	tion				Check	ked	Date	
Circle	e one:	Present	Developed					
Circle	e one:	$T_{c}$	$T_t$					
NOT	ES:	Space for a	as many as two	segments per fl	ow type can	be used f	for each wo	orksheet.
		Include a m	ap, schematic, or	r description of fl	low segments.			
Sheet f	<u>low</u> (appl	icable to T <sub>c</sub> only	)	Segment ID	)			
1.	Surface	description (tabl	e 3-1)					
2.	Mannin	g's roughness co	eff., n (table 3-1)					
3.	Flow lea	ngth, L (total L $\leq$	300 ft)	fi	ì			
4.	Two-yr	24-hr rainfall, P <sub>2</sub>	······	in	1			
5.	Land slo	ope, s		ft/f	ìt			
6.	$T_{t} = 0.0$	$07(nL)^{0.8}/P_2^{0.5}s^{0.4}$		Compute T <sub>t</sub> hr		+	=	
Shallov	v concentra	ated flow		Segment ID	)			
7.	Surface	description. (pay	ved or unpaved)					
8.	Flow lea	ngth, L		ft	;			
9.	Waterco	ourse slope, s		ft/f	ì			
10.	Average	e velocity V (figu	ıre 3-1)	ft/s	5			
11.	$T_t = L/3$	60V		Compute T <sub>t</sub> hr	r	+	=	
Channe	el flow			Segment ID	)			
12.	Cross se	ectional flow area	ı, a	ft²	2			
13.	Wetter p	perimeter, P <sub>w</sub>		ft	t			
14.	Hydraul	lic radius, r = a/P	Compute r	ft	t			
15.	Channel	l slope, s		ft/ft	t			
16.	Mannin	g's roughness co	eff., n					
17.	V = 1.49	$9 r^{2/3} s^{1/2} /n$		Compute Vft/s				
18.	Flow lea	ngth, L		ft	:	_		
19.	$T_t = L/3$	600V	Compu	te T <sub>t</sub> hr	r	+	=	
20.	Watersh	ned or subarea T <sub>c</sub>	or T <sub>t</sub> (add T <sub>t</sub> in step	os 6, 11 and 19)hr	r			

### Worksheet 4: Graphical Peak Discharge method

Project				By	_ Date
Location _			Che	ecked	Date
Circle one:	Present Develop	oed			
1. Data	a:				
Dra	inage area $A_m = $		mi <sup>2</sup> (acres/640	0)	
Run	off curve number CN =		(From worksh	eet 2)	
Tim	the of concentration $T_c = $		_ hr (From worl	sheet 3)	
Raiı	nfall distribution type = _		(I, II, III)		
Pon thro	d and swamp areas spread ughout watershed = _		percent of A <sub>n</sub>	(acres or m	i <sup>2</sup> covered)
			Storm #1	Storm #2	Storm #3
2. Frequency	·	yr			
3. Rainfall, P	(24-hour)	in			
	raction, I <sub>a</sub> vith table 4-1.)	in			
5. Compute I	/P				
6. Unit peak (Use T <sub>c</sub> an	discharge, q <sub>u</sub> d I <sub>a</sub> /P with exhibit 4)	csm/in			
7. Runoff, Q (From wor	rksheet 2).	in			
(Use percent	swamp adjustment factor, $F_p$ nt pond and swamp area with tab .0 for zero percent pond and swa	le 4-2.			
9. Peak disch (Where q <sub>p</sub>	$ \begin{aligned} &\text{marge },  q_p  \\ &= q_u A_m Q F_p) \end{aligned} $	cfs			

### Project

Worksheet 5a: Basic watershed data

Appendix
$\mathbf{C}$
ì
Exhibit
$\Pi$
(D-5)
of D
<b>%</b>

Date	
Datc	
Initial abstraction	
I <sub>a</sub> (in)	I <sub>a</sub> /P
	-
	Initial abstraction $I_a$

ተተተተ worksheet 3

ተተተተተ worksheet 2

ተተተተተ From table 5-1

Worksheet	5b:	Tabular	hy	drograph	discharge	summar

Project	Location	By	Date

Circle one: Present Developed \_\_\_\_\_\_ Frequency (yr) \_\_\_\_\_ Checked \_\_\_\_\_ Date \_\_\_\_

Subarea name	В	asic waters	hed data us	sed 1/	Select and enter hydrograph times in hours form exhibit 5- 2/2								
патіс	Sub- area	$\sum_{\mathrm{T_t}}$	I <sub>a</sub> /P	$A_mQ$									
	T <sub>c</sub> (hr)	to outlet (hr)		(mi²-in)	 Discharges at selected hydrograph times 3/(cfs)								
Composite	hydrogra	ph at outlet	:										

- $\underline{1}$ / Worksheet 5a. Rounded as needed for use with exhibit 5.
- <u>2</u>/ Enter rainfall distribution type used.

Appendix C - Exhibit II (D-6 of D-8)

 $\underline{3}$ / Hydrograph discharge for selected times in  $A_mQ$  multiplied by tabular discharge from appropriate exhibit 5.

# Worksheet 6a: Detention basin storage, peak outflow discharge (q<sub>o</sub>) known

Project	By	Date
Location	Checked	Date
Circle one: Present Developed		
Elevation or stage		
1. Data: Drainage area	Detention basin storage  6. $V_s/V_r$ (Use $q_o/q_i$ with figure 6-1)  7. Runoff, Q  (From worksheet 2)	in
2. Frequencyyr	8. Runoff volume, $V_{r} = QA_{m}53.33$	ac-ft
3. Peak inflow discharge  q <sub>i</sub>	9. Storage volume, $V_{s} = V_{r} (V_{s}/V_{r})$ $10. \text{ Maximum stage },$ $(\text{From plot})$	ac-ft
5. Compute q <sub>o</sub> / q <sub>i</sub>		

## 1/ 2<sup>nd</sup> stage q<sub>o</sub> includes 1<sup>st</sup> stage q<sub>o</sub> Appendix C - Exhibit II (D7 of D8) Appendix C - Detention basin, peak out Worksheet 6b: Detention basin, peak outflow, storage volume (V<sub>s</sub>) known

Project	By	Date
Location	Checked	Date
Circle one: Present Developed		
Elevation or stage		
1. Data:     Drainage area	Detention basin storage  6. Compute V <sub>s</sub> /V <sub>r</sub>	
2. Frequency yr	q <sub>i</sub> cfs (From worksheet 4 or 5b)	1/
3. Storage volume, V <sub>s</sub> ac ft	9. Peak outflow discharge, $q_o$ cfs $q_o = q_i (q_o/q_i)$	<u>I</u>
4. Runoff, Q in (From worksheet 2)	10. Maximum stage, $E_{max}$ (From plot)	
5. Runoff volume, $V_r$		
$\underline{1}$ / 2 <sup>nd</sup> stage $q_o$ includes 1 <sup>st</sup> stage $q_o$		

#### Appendix C - Exhibit II (D8 of D8)

#### DETENTION BASIN STORAGE DESIGN

I Calculate the peak flow in cfs due to the two year frequency storm under predeveloped conditions.

 $q_2 = A * C * i$  (allowable detention basin outflow release rate - stage one)

Intensity, "i" = 
$$a/(t_c + b)$$
 = [\_\_\_\_\_] in/hr

Where: 
$$a = 106$$
 (Table IV)

$$b = 17$$
 (Table IV)

t<sub>c</sub> = time of concentration (minutes) as determined from Appendix C - Ex. I or other acceptable means.

$$q_2 = A [ __ ] * C [ __ ] * i [ __ ] = [ __ ] cfs$$

II Calculation for the two year frequency storm under <u>post</u>development conditions.

$$Q_2 = A * C * i$$

Intensity, "i" = 
$$a/(t_c + b) = [ ___ ] in/hr$$

Where: 
$$a = 106$$

$$b = 17$$

 $t_c = time of concentration (in minutes)$ 

$$Q_2 = A [ _ ] * C [ _ ] * i [ _ ] = [ _ ] cfs$$

III Critical storm calculation.

IV Calculate maximum storm duration, T<sub>ccr</sub>, for the critical storm frequency (in minutes).

$$T_{ccr} = \left[ \frac{(A * C * a * b)}{(2 * q_2 / 3) - [(q_2^2 * t_c) / (6 * C * A * a)]} - b \right]^{1/2}$$

Where: a = determined from Table IV (for critical storm frequency)

b = determined from Table IV (for critical storm frequency)

C = the two year postdeveloped weighted runoff coefficient

A = area in acres

$$T_{ccr} = [\underline{\hspace{1cm}}]$$
 minutes

IV Calculate I<sub>cr</sub>.

$$I_{cr} = [a / (T_{ccr} + b)] = [\underline{\hspace{1cm}}] in/hr$$

V Calculate Q<sub>cr</sub>, flow at maximum duration for the critical storm frequency:

$$Q_{cr} = A[\_\_] * C[\_\_] * I_{cr}[\_\_] = [\_\_] cfs$$

VI Calculate the required storage volume due to critical storm criteria, SV<sub>cr</sub>:

$$SV_{cr} = (60 * Q_{cr} * T_{ccr}) - \{ [2 * q_2 * (T_{ccr} + t_c) * 60] / 3 \} + [ (q_2^2 * t_c * 60) / (6 * Q_{cr}) ]$$

$$SV_{cr} = [ _{max}] ft^3$$

VII Calculate the peak flow in cfs due to the one-hundred year frequency storm under <u>pre</u>developed conditions.

 $q_{100} = A * C * i$  (allowable detention basin outflow release rate - stages one + two)

Runoff Coefficient, "C" = [\_\_\_\_]

Intensity, "i" =  $a / (t_c + b) = [ ___ ] in/hr$ 

Where: a = 290 (Table IV)

b = 31 (Table IV)

t<sub>c</sub> = time of concentration (minutes) as determined from Appendix C - Ex. I, for predeveloped

$$q_{100} = A [ \_ ] * C [ \_ ] * i [ \_ ] = [ \_ ] cfs$$

VII Calculate maximum storm duration  $T_{c100}$ , for the one-hundred year frequency (in minutes) storm under postdeveloped conditions.

Appendix C - Exhibit III (2 of 4)

$$T_{c100} = \left[ \frac{(A * C * a * b)}{(2 * q_{100} / 3) - [(q_{100}^{2} * t_{c}) / (6 * C * A * a)]} \right]^{\frac{1}{2}} - b$$

Where: a = 290

b = 31

c = the one-hundred year <u>post</u>developed weighted runoff coefficient

A = area in acres

$$T_{c100} = [\underline{\phantom{a}}]$$
 minutes

VIII Calculate I<sub>100</sub>:

$$I_{100} = [a/(T_{c100} + b)] = [\underline{\hspace{1cm}}] in/hr$$

IX Calculate  $Q_{100}$ ; the flow at maximum duration for the one-hundred year storm frequency.

$$Q_{100} = a [ \_ ] * C [ \_ ] * I_{100} [ \_ ] = [ \_ ] cfs$$

X Calculate  $SV_{100}$ ; the storage volume required due to the one-hundred year storm.

$$SV_{100} = (60 * Q_{100} * T_{c100}) - \{ [2 * q_{100} * (T_{c100} + t_c) * 60] / 3 \} + [(q_{100}^2 * t_c * 60 / (6 * Q_{100})]$$

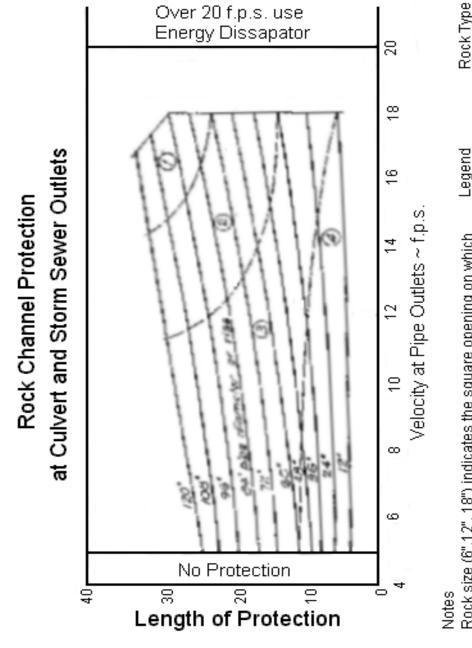
#### XI Design Notes:

- 1. Design as a **two stage** outlet
  - 1. An iterative process is required since the change in elevation head will cause an increase in the outflow of the stage one opening.
  - 2. Two detention areas can be used to eliminate the iterative two stage outlet design process.
  - 3. If a one stage outlet is to be used that cannot detain the 100 year storm and release at the 2 year predeveloped rate, explain reasoning.
- 2. Emergency overflow must be accounted for via a spillway or other means.

#### General Notes:

1. The formulas used in calculations III through VI assume an <u>orifice</u> controlled outflow condition.

Appendix C - Exhibit III (3 of 4)
Reference pages 98 and 99, <u>Water and Wastes Engineering</u>, "Estimate Detention and Reservoir Storage". By A. S. Paintal, P.E., Ph.D. 2.



48" of 18" rock 36" of 18" rock 30" of 12" rock લંલ <del>ક</del> Rock size (6",12", 18") indicates the square opening on which Minimum width of protection shall be twice the pipe (Where a stream bed will withstand the calculated 85% of the material by weight will be retained. diameter, with 4" being the very minimum.

a( a( ID )

(where a sugarn ped will will stand the calculated velocity without erosion, no rock channel protection will be required.)

C C N L O C O C R

#### Appendix C - Exhibit IV

#### CRITICAL AREA PLANTING

#### 1. TEMPORARY AND PERMANENT SEEDING

#### 1.1 SEEDBED PREPARATION

- A.Lime (in lieu of a soil test recommendation) on acid soil (ph = 5.5 or less) and subsoil at a rate of 100 pounds per 1000 sq. ft. or two (2) tons per acre of agricultural ground limestone.
- B.**Fertilizer** (in lieu of soil test recommendation) shall be applied at a rate of 12-15 pounds (25 pounds for permanent seeding) per 1000 sq. ft. of 10-10-10 or 12-12-12 analysis or equivalent.

#### 1.2SEEDING

#### A.Species Selection

#### (1)Temporary Seeding Mixture

Seeding Period	<u>Type</u>	<u>Rate</u> (1000 ft <sup>2</sup> )
Spring and	1. Oats	3 lbs
Summer	2. Peren. Ryegrass	1 lbs
	3. Tall Fescue	1 lbs
Fall	1. Peren. Ryegrass	1 lbs
	2. Rye	3 lbs
	3. Wheat	3 lbs
	4. Tall Fescue	1 lbs

#### (2) Permanent Seeding Mixture

Seeding Period	<u>Type</u>	$\underline{\text{Rate}} \ (1000 \ \text{ft}^2)$
Spring,	1. Creeping Red Fescue	0.5 lbs

Summer, and	Domestic Ryegrass	0.25 lbs
Fall	Kentucky Bluegrass	0.25 lbs
	2. Tall Fescue	1 lbs
	3. Dwarf Fescue	1 lbs

#### Appendix D - Exhibit I (1 of 3)

#### (2-1) Seedings for Steep Banks or Cuts

Spring,	1. Tall Fescue	1 lbs
Summer, and		
Fall	2. Crownvetch	0.25 lbs
	Tall Fescue	0.50 lbs
	3. Flatpea	0.50 lbs
	Tall Fescue	0.50 lbs

(2-2) Seedings for Waterways and Road Ditches

Spring, 1. Tall Fescue 1 lbs
Summer, and
Fall

- B. Apply the seed uniformly with a cyclone seeder, drill, cultipacker seeder, or hydroseeder (slurry may include seed and fertilizer) preferably on a firm, moist seedbed. Seed wheat or rye no deeper than one (1) inch. Seed ryegrass no deeper than one quarter (1/4) of an inch.
- C. When feasible, except where a cultipacker type seeder is used, the seedbed should be firmed following seeding operations with a cultipacker, roller, or light drag. On sloping land seeding operations should be on the contour wherever possible.
- D. Other seed species may be substituted for these mixtures.
- E. These seeding rates need to be increased two to three times if they are to be used as a lawn.

#### 2. DORMANT SEEDING

A. Temporary Seeding - After November 1, use mulch only.

- B. Permanent Seeding Seedings should not be planted from October 1 through November 20. The following methods may be used to make a "dormant seeding":
  - (1) From October 1 through November 20, prepare the seedbed, add the required amounts of lime and fertilizer, then mulch and anchor. After November 20, and before March 15, broadcast the selected seed mixture. Increase the seeding rates by 50 percent for this type of seeding.
  - (2) From November 20 through March 15, when soil conditions, permit, prepare the seedbed, lime and fertilize, apply the selected seed mixture, and

Appendix D - Exhibit I (2 of 3)

(3) mulch and anchor. Increase the seeding rates by 50 percent for this type of seeding.

#### 3. <u>MULCHING</u>

- A. Mulch shall consist of small grain straw (preferably wheat or rye) and shall be applied at the rate of two tons per acre or 100 pounds per 1000 sq. ft.
- B. Spread the mulch uniformly by hand or mechanically so the soil surface is covered.

#### C. Mulch Anchoring Methods

- (1) <u>Mechanical</u> Use a disk, crimper, or similar type tool set straight to punch or anchor the mulch material into the soil.
- (2) <u>Asphalt Emulsion</u> Apply at the rate of 160 gallons per acre into the mulch as it is being applied.
- (3) <u>Mulch Netting</u> Use according to the manufacturer's recommendations.

#### 4. IRRIGATION

Supply new seedlings with adequate water for plant growth until they are firmly established.